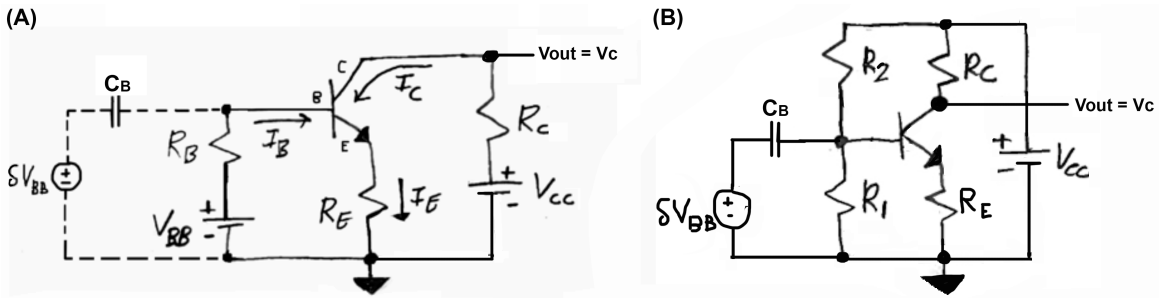


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### Physics 120 - Final exam - 14 June 2018

Complete the design of the common emitter transistor amplifier using a 2N3904 NPN BJT, demonstrate that it operates as planned in terms of gain, dynamic range, and bandwidth.



The left hand loop (**Fig. A**)

$$-V_{BB} + I_B R_B + V_{BE} + I_E R_E = 0$$

but  $I_B = \frac{1}{\beta} I_C$  and  $I_E = \frac{1+\beta}{\beta} I_C$

so  $I_C = \frac{\beta}{1+\beta} \frac{V_{BB} - V_{BE}}{R_E + R_B/(1+\beta)}$

Recall that  $\beta \gg 1$  ( $\beta \sim 100$  in this case) and choose  $R_B \ll (1+\beta)R_E$ . Then

$$I_C \approx \frac{V_{BB} - V_{BE}}{R_E}$$

**Gain:** The output voltage is given by

$$V_C = V_{CC} - I_C R_C = V_{CC} - \frac{V_{BB} - V_{BE}}{R_E} R_C = \left( V_{CC} + \frac{R_C}{R_E} V_{BE} \right) - \frac{R_C}{R_E} V_{BB}$$

The output is equal to the collector voltage,  $V_C$ , and is linear in  $V_{BB}$ . The voltage  $V_{BB}$  contains a constant as well as a signal component,  $\delta V_{BB}$  (**Fig. A,B**). The change  $\delta V_{BB}$  leads to a proportional change in the output,  $\delta V_C$ , i.e.,

$$\delta V_C \approx -\frac{R_C}{R_E} \delta V_{BB} \text{ where the ratio } "- R_C / R_E" \text{ is the voltage gain of the circuit.}$$

**Load line:** The set-point, denoted  $I_{C,Q}$  and  $V_{CE,Q}$ , are the values of  $I_C$  and  $V_{CE}$  with  $\delta V_{BB} = 0$ . The value of  $V_{CE}$  is bounded at by  $V_{CE,Sat} = 0.2 \text{ V}$  and  $V_{CC} = 15 \text{ V}$ .

**Design constraints:**

Choose  $V_{CEQ} = V_{CC}/2$  to insure a (near) maximum voltage swing.

Choose  $I_{CQ} = 10 \text{ mA}$ , the optimum current for this BJT

Choose  $|\text{Gain}| = 10$ , so  $R_C = 10 R_E$

Satisfy the load-line relation  $I_{CQ} \approx \frac{V_{CC} - V_{CEQ}}{R_E + R_C} \approx \frac{V_{CC}}{2R_C}$ , which yields  $R_C \approx \frac{V_{CC}}{2I_{CQ}}$ .

Satisfy the constraints  $R_B \ll \beta R_E$ . Since  $\beta \geq 100$ , select  $R_B = 10 R_E$ .

Calculate  $V_{BB} \approx V_{BE} + I_{C,Q} R_E$ .

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**Realization** (*note: confirm the value of all components prior to construction*)

(1a-c) Pick standard values of resistors:

$$R_C \approx 750 \Omega$$

$$R_E \approx 75 \Omega$$

$$R_B \approx 750 \Omega$$

(1d) Calculate  $V_{BB}$ :

$$V_{BB} \approx 1.2 \text{ V}$$

Convert from dual to single power supply with a voltage divider (**Fig. B**) to replace  $V_{BB}$  and  $R_B$ :

$$R_B \approx \frac{R_1 R_2}{R_1 + R_2} \quad \text{and} \quad V_{BB} \approx \frac{R_1}{R_1 + R_2} V_{CC} \quad \text{so that} \quad R_1 \approx R_B \frac{V_{CC}}{V_{CC} - V_{BB}} \quad \text{and} \quad R_2 \approx R_B \frac{V_{CC}}{V_{BB}}$$

(1e,f) Pick standard values of resistors:

$$R_1 \approx 810 \Omega$$

$$R_2 \approx 10 \text{ k}\Omega$$

(1g) Show that your choice satisfies  $R_1 \ll R_{\text{input}}$ , i.e.,  $R_1 \ll \beta R_E$ , so that the input resistance does not contribute to the voltage divider.

$$810 \Omega \ll 100 \cdot 75 \Omega = 7500 \Omega$$

**Testing** (*recall: the oscilloscope and DMM inputs are not differential*)

(2a) Measure and record the actual value of  $V_{CE,Q}$  (how?):

$$V_{CE,Q} \approx \text{(Call for a TA to demonstrate your measurement)}$$

**Differential voltage from collector to emitter. This could be successive measurements.**

(2b) Measure and record the actual value  $I_{C,Q}$  (how?):

$$I_{C,Q} \approx \text{(Call for a TA to demonstrate your measurement)}$$

**Series current along collector OR along emitter leg OR via voltage drop across  $R_C$  or across  $R_E$ . Drop across  $R_E$  is a single probe measurement and simplest.**

(2c) Pick a standard value of capacitor, or combined capacitors, to couple  $\delta V_{BB}$  through a high-pass filter with cut-on frequency of  $f_{\text{High-pass}} \sim 1.0 \text{ kHz}$  (**Fig A,B**) (*recall:  $f_{\text{High-pass}} = 1/(2\pi R_B C_B)$* ):

$$C_B \approx 0.21 \mu\text{F} \quad \text{OR} \quad \text{two } 0.1 \mu\text{F} \text{ capacitors in parallel}$$

(2d) Show that the output  $\delta V_C$  spans the full range of positive and negative values of  $\delta V_{BB}$  for an  $\sim 1 V_{\text{peak-to-peak}}$  sine input at  $\sim 10 \text{ kHz}$  (*note: ensure  $Z_{\text{out}} = \text{High}$  for the function generator*).

**Call for a TA to observe your demonstration (show  $\delta V_{BB}$  and  $\delta V_C$  on the oscilloscope)**

(2e) Measure the output  $\delta V_C$  as a function of frequency (*hint: use "AC" coupling on the oscilloscope for ease*). What is the actual value of the cut-on frequency, i.e.,  $f_{3\text{dB}}$  for high-pass?

$$f_{\text{High-pass}} \approx$$

(2f) What is the value of the cut-off frequency, i.e.,  $f_{3\text{dB}}$  for low-pass?

$$f_{\text{Low-pass}} \approx$$

(2g) What is the origin of the high-frequency filtering for  $f_{\text{Low-pass}}$ ?

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